

Iowa Title V Operating Permit Control Efficiency Table

| Control Device or Practice | Control Efficiency (%) | | | | | | |
|--|------------------------|------------------|-----------------|-----------------|-----------------|----|-----------------|
| | TSP | PM ₁₀ | SO _x | NO _x | VOC | CO | Pb |
| Wet Scrubber - high efficiency | note 1 | | note 2 | | | | |
| Wet Scrubber - med efficiency | note 1 | | note 2 | | | | |
| Wet Scrubber - low efficiency | note 1 | | note 2 | | | | |
| Gravity Collector | 3 ^a | -- | -- | -- | -- | -- | 2 ^a |
| Centrifugal Collector (cyclone)-high efficiency* | 95 ^c | 80 ^a | -- | -- | -- | -- | 65 ^a |
| Centrifugal Collector (cyclone)-med efficiency* | 75 ^c | 50 ^a | -- | -- | -- | -- | 40 ^a |
| Centrifugal Collector (cyclone)-low efficiency* | 35 ^c | 10 ^a | -- | -- | -- | -- | 8 ^a |
| Electrostatic Precipitator-high efficiency ** | 95 ^a | 95 ^a | -- | -- | -- | -- | 75 ^a |
| Electrostatic Precipitator-medium efficiency ** | 80 ^a | 80 ^a | -- | -- | -- | -- | 65 ^a |
| Electrostatic Precipitator-low efficiency ** | 70 ^a | 70 ^a | -- | -- | -- | -- | 55 ^a |
| Fabric Filter | 99 ^a | 95 ^c | -- | -- | -- | -- | 80 ^a |
| Catalytic Afterburner | -- | -- | -- | -- | 95 ^c | -- | -- |
| Direct Flame Afterburner | -- | -- | -- | -- | 95 ^c | -- | -- |
| Flaring | -- | -- | -- | -- | 90 ^a | -- | -- |
| Low NO _x Burners | -- | -- | -- | note 3 | -- | -- | -- |
| Staged Combustion | -- | -- | -- | 40 ^a | -- | -- | -- |
| Flue Gas Recirculation | -- | -- | -- | 50 ^a | -- | -- | -- |
| Reduced Combustion Air Preheat | -- | -- | -- | note 4 | -- | -- | -- |
| Steam or Water Injection | -- | -- | -- | 65 ^a | -- | -- | -- |
| Low Excess Air Firing | -- | -- | -- | 30 ^a | -- | -- | -- |
| Fuel with low Nitrogen Content | -- | -- | -- | 50 ^a | -- | -- | -- |
| Sulfuric Acid Plant-Single Contact Process | -- | -- | 50 ^a | -- | -- | -- | -- |
| Sulfuric Acid Plant-Double Contact Process | -- | -- | 95 ^a | -- | -- | -- | -- |
| Vapor Recovery System (Condensers) | -- | -- | -- | -- | note 5 | -- | -- |
| Activated Carbon Adsorption | -- | -- | note 6 | | | | -- |
| Gas Absorption Column-packed | 90 ^a | 90 ^a | note 2 | | | | -- |
| Gas Absorption Column-tray type | 25 ^a | 25 ^a | note 2 | | | | -- |
| Spray Tower | 20 ^a | 20 ^a | note 2 | | | | -- |
| Venturi Scrubber | 90 ^a | 90 ^a | note 2 | | | | -- |

Control Efficiency Table (continued)

(continued)

| Control Device or Practice | Control Efficiency (%) | | | | | | |
|--|------------------------|------------------|-----------------|-----------------|-----|----|-----------------|
| | TSP | PM ₁₀ | SO _x | NO _x | VOC | CO | Pb |
| Impingement Plate Scrubber | note 7 | | -- | -- | -- | -- | -- |
| Mat or Panel Filter | 90 ^c | 90 ^c | -- | -- | -- | -- | -- |
| Dust Suppression by Water Spray | 40 ^a | 40 ^a | -- | -- | -- | -- | -- |
| Dust Suppression by Chemical or Wetting Agents | 40 ^a | 40 ^a | -- | -- | -- | -- | -- |
| Catalytic Reduction | -- | -- | -- | note 8 | -- | -- | -- |
| Wet Lime Slurry Scrubbing | -- | -- | 85 ^c | -- | -- | -- | -- |
| Multiple Cyclone w/o Fly Ash Reinjection | 80 ^a | 80 ^a | -- | -- | -- | -- | 65 ^a |
| Multiple Cyclone with Fly Ash Reinjection | 50 ^a | 50 ^a | -- | -- | -- | -- | 40 ^a |
| Water Curtain | 50 ^c | 10 ^a | -- | -- | -- | -- | -- |

^a – Control efficiency was taken from a literature review and developmental work by the Minnesota Pollution Control Agency

^b – Control efficiency was taken from AP-42

^c – Control efficiency was developed from the combination of a literature review and developmental work by the Minnesota Pollution Control Agency, AP-42, and staff judgment

* Low, medium, and high efficiency cyclones will be defined based on pressure drop. The ranges of pressure drops are as follows:

| | |
|----------------------------|-------------------|
| Low-efficiency cyclones | 2-4 inches water |
| Medium-efficiency cyclones | 4-7 inches water |
| High-efficiency cyclones | 7-10 inches water |

** Low, medium, and high efficiency electrostatic precipitators (ESP) will be defined based on the specific collection area (SCA). The SCA is the total collector plate area divided by the gas volume flow rate. It is usually expressed in terms of square feet per 1000 acfm of gas flow. For example, the SCA of an ESP with a gas flow rate of 250,000 acfm and collection plate area of 100,000 square feet is:

$$100,000 \text{ ft}^2 / 250,000 \text{ acfm} \times 0.001 = 400 \text{ ft}^2/\text{thousand acfm}$$

The ranges of SCA for low, medium, and high efficiency ESPs are as follows:

| | |
|-----------------------|-----------|
| Low-efficiency ESP | < 400 |
| Medium-efficiency ESP | 400 - 700 |
| High-efficiency ESP | > 700 |

Typical control efficiencies were not assigned to all control devices because some efficiencies strongly depend on source specific parameters. In these instances the table will refer to one of the notes listed below for additional information.

Note 1. Particulate control equipment represented by these classifications should be included in the other, more specific categories (i.e., venturi scrubbers or packed bed absorption columns).

Note 2. The achievable gaseous pollutant control efficiencies for these types of control equipment will depend on the pollutant solubility, the solvent used, the vapor- liquid contact time, and the contact area. These devices are normally designed to achieve a promulgated control efficiency rather than the maximum achievable reduction. Control efficiencies for these devices should be evaluated on a case-by- case basis.

Note 3. Low NO_x burners (LNB) have been developed by many boiler and burner manufacturers for both new and retrofit applications. Low NO_x burners limit NO_x formation by controlling both the stoichiometric and temperature profiles of the combustion process. This control is achieved with design features that regulate the aerodynamic distribution and mixing of the fuel and air, yielding one or more of the following conditions:

1. Reduced O₂ in the primary combustion zone, which limits fuel NO_x formation;
2. Reduced flame temperature, which limits thermal NO_x formation; and
3. Reduced residence time at peak temperature, which limits thermal NO_x formation.

The amount of NO_x reduction achievable is dependent upon the combustion system and burner design, actual operating practices, and fuel characteristics. The amount of reduction should be based on the manufacturer's demonstration.

Note 4. The amount of NO_x reduction achievable from reducing preheating of combustion air will vary according to the temperatures before and after the modification. Therefore, efficiencies for this process should be evaluated on a case-by-case basis.

Note 5. Control efficiencies for a particular condenser will vary for different VOC compounds and depends on both the partial pressure of the pollutant and the operating parameters of the condenser. Efficiencies should be evaluated on a case- by-case basis.

Note 6. Since the overall control efficiency will depend on source specific parameters such as the physical characteristics of the absorbent bed and gaseous stream, the temperature, and the choice of regeneration technique, efficiencies should be evaluated on a case-by-case basis.

Note 7. Depending on the application control efficiencies may range from 25-99%. Efficiencies should be evaluated on a case-by-case basis.

Note 8. Generic classification; recommend specific technologies be addressed on an individual basis. Two widely used NO_x control technologies include Selective Catalytic Reduction (SCR) and Selective Noncatalytic Reduction (SNCR). SCR can obtain reductions of 60-90%. Urea based SNCR can achieve reductions of 30-80% and ammonia based 55-85%.