

DATE RECEIVED		FACILITY NAME		COUNTY No.	PROGRAM AREA CODE	FACILITY TYPE CODE	SUBJECT AREA CODE
12/2/87		Lohrville Wastewater Treatment Facility		13	2P	CO4	16.3.1 325
RULE REFERENCE	DESIGN STANDARD REFERENCE	DECISION		APPEAL ACTION		DATE	
9 567-64.2(9)	10 16.3.1	11 Approved 12/23/87		12			
ENGINEER				VARIANCE RULE			
13 Veenstra & Kimm				14 64.2(9) "c"			

15. DESCRIPTION OF VARIANCE REQUESTED:

The engineer requests a variance to provide an 8 foot sidewater depth for the final clarifier following a trickling filter instead of the 10 foot depth required by the standards.

16. ENGINEERS JUSTIFICATION: A new final clarifier is proposed in lieu of an equalization basin to construct the project within the available funds. However, space for the tank is limited, the site is steeply sloped and there is a high groundwater table. Excavation will be 20 feet deep, and it would be difficult to go any deeper without encroaching on adjacent property. The engineer feels that use of an 8 foot depth for the final clarifier will provide satisfactory treatment even at PHWW flows which are more than 10 times greater than AWW flows. The proposed final clarifier would be circular.

17. DEPARTMENTS JUSTIFICATION: West Union requested variance for 8 foot depth for a rectangular tank to match existing tank, claiming it worked in Independence. The request was denied.

Atalissa requested a variance for rectangular tank using I & A proprietary Aero-Med process designed for 8 foot depth. The request was approved.

Two others approved were small private projects. It appears that this variance would provide substantially equivalent effectiveness while significantly reducing costs and we recommend that it be approved.

18. PRECEDENTS USED: Heartland Lysine - Approved
West Union - Denied
Atalissa - Approved
Risen Sun Christ. Vill. - Approved

19. STAFF REVIEWER: Wayne A. Reed
20. SUPERVISOR: Larry Haag approved 12/1/82
21. AUTHORIZED BY: Donell H. Allst - approved 12/23/87

to: Varian
Ann. Log

1/11/57

C. Lockville Variance request.

Since the peak hour flow is ten times the average wet weather flow and the clarifier diameter is determined in this case, by the peak hour flow, 94-95% of the time the surface overflow rates will be much lower than the design standards require. The lower surface overflow rate will compensate for the lesser depth. At the average wet weather flow the surface overflow rate will be 120 gal/day/ft² compared to a design standard of 600 gal/day/ft². With mechanical sludge removal, I would not project any problems with the sludge causing problems in the effluent.

Wayne Parrand told me that when they dealt with West Union, they could not find any literature to justify for intermediate ^{10 ft. over 8 ft.} The design standard ~~for~~ ^{for} clarifiers following trickling filters only require 7 ft of depth.

The reasoning for the variance request at West Union, was (1) the potential problem of hitting rock and (2) the existing Clarifiers were 8 ft. deep and they were using common wall construction. These Clarifiers were rectangular.

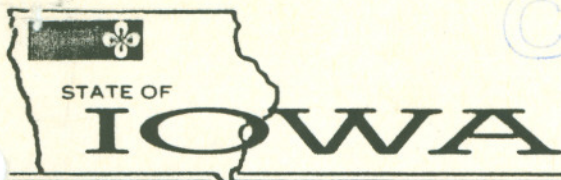
My reasoning to grant the variance
is because of the wide variation in
peak flow and average wet weather
flows and because the construction is
quite deep plus the fact they
would run into ground water.

12/3/87

Wayne: Off the top, I
don't have a problem
with their request but
if we grant the variance,
we should include a
stipulation that if it
doesn't work properly,
baffling or other remedies
will be done to solve problems.

Would you prepare
the variance form
according to your
judgement

SH



TERRY E. BRANSTAD, GOVERNOR

COPY

RECORD COPY

File Name Lohrville Sewage

Senders Initials WAP

DEPARTMENT OF NATURAL RESOURCES

LARRY J. WILSON, DIRECTOR

December 30, 1987

City of Lohrville
City Hall
Lohrville, IA 51453

PROJECT NO.: S87-210
FILE: Lohrville - Sewage
SUBJECT: Wastewater Treatment Facility

Gentlemen:

The Iowa Department of Natural Resources in accordance with Subrule 567--64.2(9)c of the Iowa Administrative Code has approved your request for a variance from Iowa Wastewater Facilities Design Standard 16.3.1 which requires that final settling tanks following fixed film reactors shall have a minimum sidewater depth of ten feet.

The engineering justification submitted substantially demonstrates that this variance will result in at least equivalent effectiveness while significantly reducing costs.

Sincerely,

DARRELL McALLISTER
BUREAU CHIEF
SURFACE AND GROUNDWATER PROTECTION BUREAU

DM/mjt/M364MJT.4

cc: Veenstra & Kimm, Inc.
Field Office 3

Distribution

1 Engineer; 1 Field Office; 1 DNR File



VEENSTRA & KIMM, INC.
CONSULTANT GROUP

November 30, 1987

Lavoy Haage
Iowa Department of Natural Resources
Henry A. Wallace Building
900 East Grand Avenue
Des Moines, Iowa 50319

LOHRVILLE, IOWA
WASTEWATER TREATMENT FACILITY IMPROVEMENTS

In accordance with discussions between Harvey Gullicks of Veenstra & Kimm, Inc., and Lavoy Haage and Wayne Reed of IDNR, we are requesting a variance for construction proposed for the above project. The requested variance is for construction of a 30-foot diameter final clarifier with 8-foot side water depth in lieu of the construction of a flow equalization pond/tank.

Flows up to 175,000 to 200,000 gallons per day are to be directed through the Imhoff tank, trickling filter and into the final clarifier. Greater flows are to be routed to bypass the Imhoff tank and trickling filter, but will be routed through final clarification. We propose to keep the existing rectangular final clarifier in service to reduce the affects of wet weather flows. The new and existing final clarifiers will have a capacity capable of handling the peak hour wet weather flow at surface overflow rates of 1,500 gallons per square foot per day.

Construction of the larger final clarifier represents the best economical alternative available to the City of Lohrville for compliance with the IDNR mandated completion of improvements for the wastewater treatment facility. The 8-foot side water depth is requested because of the high groundwater table, ground surface topography, and construction-related areal constraints.

Your timely response to our request for discussions of construction alternatives on November 23, 1987 was greatly appreciated.

VEENSTRA & KIMM, INC.

A handwritten signature in cursive script that reads "Harvey A. Gullicks".

Harvey A. Gullicks, P.E., Ph.D.

HAG:jgt
2474
cc: Doneta Nelsen, City Clerk

IOWA DEPARTMENT OF WATER, AIR AND WASTE MANAGEMENT

WATER QUALITY

CONSTRUCTION PERMIT APPLICATION

PROGRAM

SCHEDULE F, TREATMENT PROJECT SITE SELECTION

WAWM USE

DATE PREPARED
February 5, 1988PROJECT IDENTITY
City of Long Grove
Treatment System Improvements

PROJECT NO.

DATE REVISED

PERMIT NO.

1. Project Location: County Scott Section 34 Township 80N Range 3EIs this a new site? Existing site? X or Expansion of existing site?

2. Provide the following as attachments (minimum of three each needed):

(a) General Plat Layout of area within a 5 mile radius of the project, noting all important features.
(U.S.G.S. map may be used.)

(b) Site Layout of area within a 1,500 foot radius of the project.

3. Does the project lie in a flood plain? Yes No XElevation of 100 year flood (MSL) 715.18 Elevation of 25 year flood (MSL) 713.18Will the treatment works structures, including the electrical and mechanical equipment, be protected from physical damage by the 100 year flood? Yes X No Will the plant remain operational during the 25-year flood? Yes X No Method of flood protection Top of dykes at 736.54. Minimum distance to high water table 10.32 feet5. Describe geology of area Glacial till - gently rolling6. Describe soil conditions Stiff to medium stiff silty clay with 1 - 2 ft. of topsoil

7. State the minimum distances and direction to:

(a) Municipal wells 2300 ft.(b) Private wells 600 ft.(c) Residences or Businesses 300 ft.(d) Recreation areas 1,000 ft.(e) Other 8. Direction of the prevailing winds West-Southwest9. Sulfate content of the raw water supply source 84 mg/l. Identify source City Records10. Is this area available for expansion? Yes No X. If yes, how much? Location of area
Identify owner of property 11. Will site be accessible via an all weather access road? Yes X No
Type Gravel

12. Source of STP water supply:

Maintenance/Cleanup None Potable? Yes No Laboratory/Sanitary None Potable? Yes No Potable? Yes No 13. Receiving Stream Mason Mason Creek tributary to Wapsipinicon River
7-day 10-year Low Flow NA cfs. Source of stream flow data
Drainage area above site 0.18 square miles
Is stream a dry run Yes Intermittent continuous flow
Describe downstream usage of the receiving stream None

27

26

Scale
1" = 1,000'

Long Grove

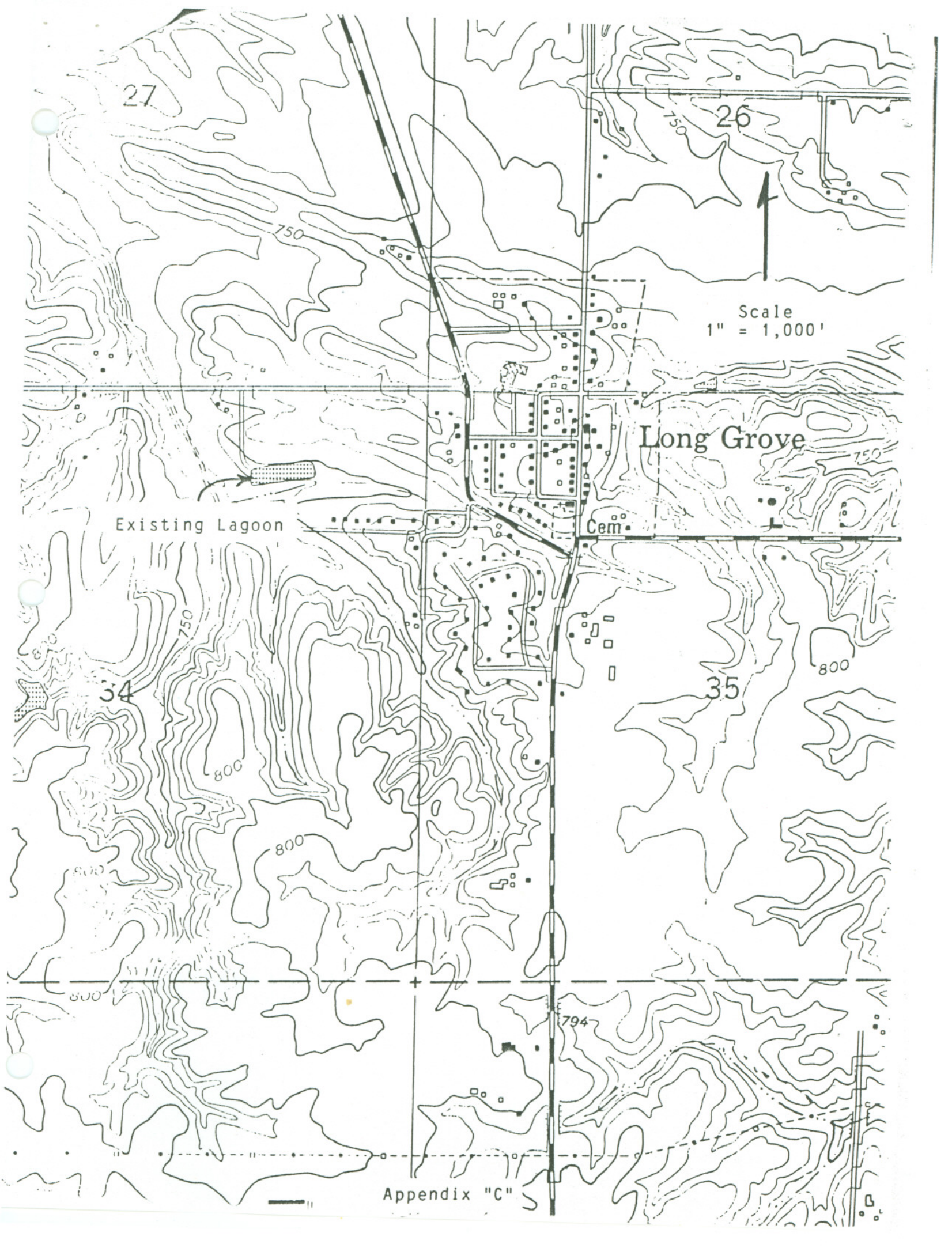
Existing Lagoon

Cem

34

35

Appendix "C"



IOWA DEPARTMENT OF WATER, AIR AND WASTE MANAGEMENT

WATER QUALITY

CONSTRUCTION PERMIT APPLICATION

PROGRAM

SCHEDULE G, TREATMENT PROJECT DESIGN DATA

WAWM USE

DATE PREPARED

PROJECT IDENTITY

PROJECT NO.

February 5, 1988

City of Long Grove

DATE REVISED

Treatment System Improvements

PERMIT NO.

1. Project Description Modification of an existing 180 day single cell lagoon system to create an aerated lagoon.

2. Design Basis:

Plant Design Loading		Present			Design Year ()		
		ADW	AWW	MWW	ADW	AWW	MWW
Residential Waste	Population		////////	////////	500	////////	////////
	Flow, MGD						
	BOD ₅ , #/day						
	TKN, #/day						
Out of Town Students	Number		////////	////////		////////	////////
	Flow, MGD						
	BOD ₅ , #/day						
	TKN, #/day						
Industrial	Flow, MGD						
	Rated Flow, MGD						
	BOD ₅ , #/day						
	TKN, #/day						
Other (Specify)	Flow, MGD						
	Rated Flow, MGD						
	BOD ₅ , #/day						
	TKN, #/day						
Infiltration	MGD						
Inflow	MGD						
Total	Flow, MGD				.040	.060	.090
	Rated Flow, MGD						
	BOD ₅ , mg/l				255	170	113
	BOD ₅ , #/day				85	85	85
	TKN, mg/l				39	26	17
	TKN, #/day				13	13	13

3. Peak Hourly Dry Weather Flow .06 MGD + Peak Hourly Infiltration .024 MGD + Peak Hourly Inflow .006 MGD = Total Peak Hourly Wet Weather Flow .090 MGD (In Design Year)

4. Identify effluent limitations

BOD 5 day	Suspended Solids	NH ₃ -N					
		Avg	Max	Avg	Max	Avg	Max
Operation Permit	mg/l	25	40	80	120		
Effluent Limits	#/day						
Design Effluent	mg/l	25	40	38	120		
Quality	#/day						

5. Identify significant industrial/commercial contributors:

Waste Contributors	Pre-treat	Operation		Design Loadings						
		Hrs Day	Days Week	Flow MGD		BOD ₅ #/day	Susp. Solids #/day	TKN #/day	Oil & Grease #/day	#/day
				Total	Rated					

IOWA DEPARTMENT OF WATER, AIR AND WASTE MANAGEMENT

CONSTRUCTION PERMIT APPLICATION

WATER QUALITY
PROGRAM

DATE PREPARED
2/4/88

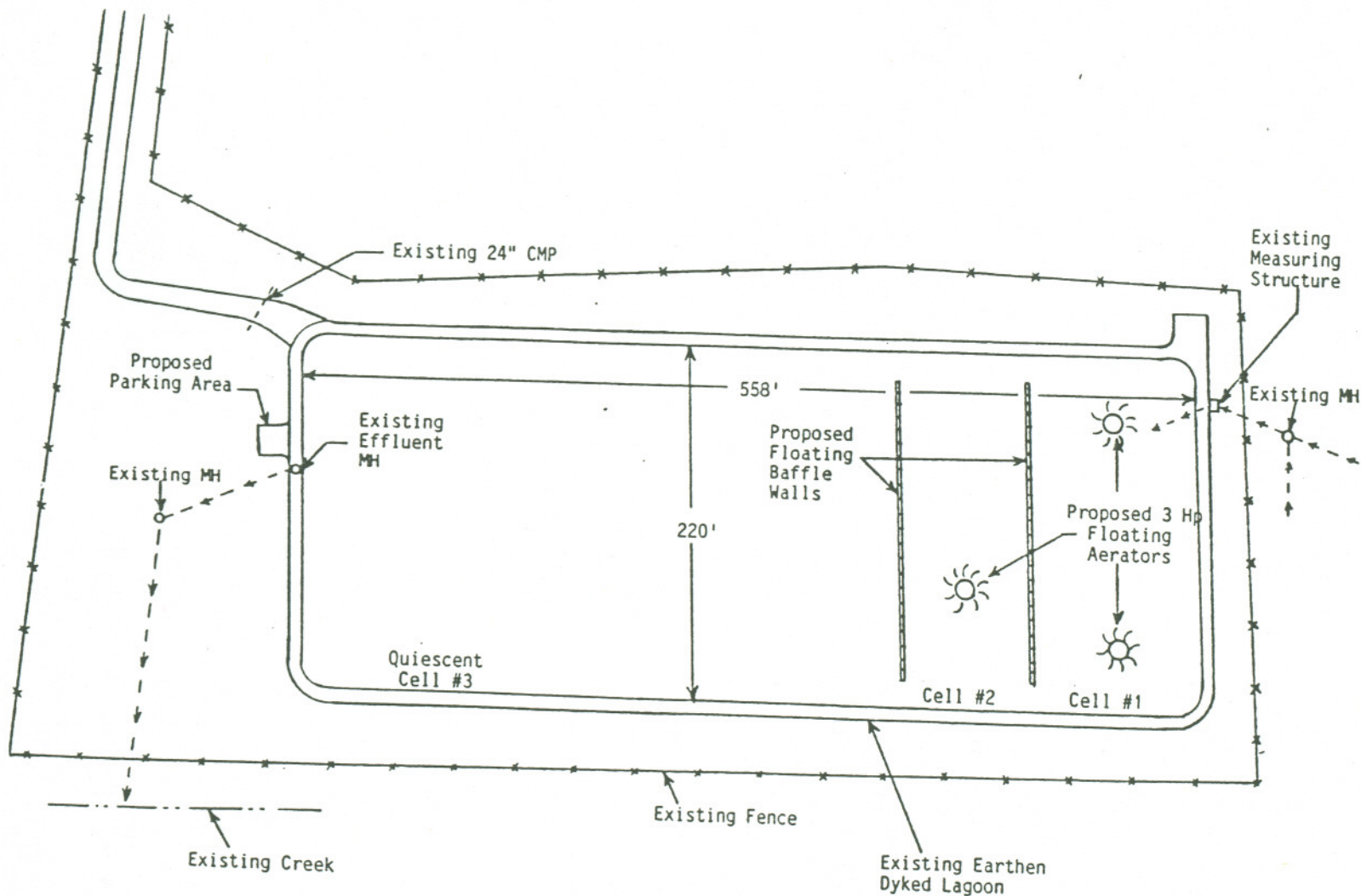
DATE REVISED

SCHEDULE H1, SCHEMATIC FLOW DIAGRAM

PROJECT IDENTITY
City of Long Grove
Treatment System Improvements

MAWM USE
PROJECT NO.

PERMIT NO.



IOWA DEPARTMENT OF WATER, AIR AND WASTE MANAGEMENT

WATER QUALITY		CONSTRUCTION PERMIT APPLICATION		
PROGRAM		SCHEDULE H2, TREATMENT PROCESS REMOVAL EFFICIENCY		WAWM USE
DATE PREPARED February 5, 1988		PROJECT IDENTITY City of Long Grove Treatment System Improvements		PROJECT NO.
DATE REVISED				PERMIT NO.

1. Project:

A. Design Basis:

ADW - 040 MGD
 AWW - 060 MGD
 MWW - 090 MGD
 PHWW - 090 MGD

Design Temperature - 1° C Winter

B. Iowa Operation Permit

Effluent Limits:

	Monthly Average*		Daily Maximum	
	mg/l	#/day	mg/l	#/day
CBOD ₅	<u>25</u>	<u> </u>	<u>40</u>	<u> </u>
TSS	<u>80</u>	<u> </u>	<u>120</u>	<u> </u>
NH ₃ -N	<u> </u>	<u> </u>	<u> </u>	<u> </u>

*with a minimum monthly average removal rate of %

2. Processes - at Design Flow of 0.048 MGD

	AWW			MWW			
	mg/l	#/day	% removal	mg/l	#/day	% removal	
A. Primary treatment - description:							
CBOD ₅	212	85	60				Cell No. 1
TSS	249	100	80				
NH ₃ -N							
B. Secondary treatment - description:							
CBOD ₅	85	34	70				Cell No. 2
TSS	50	20	25				
NH ₃ -N							
description:							
BOD ₅							
TSS							
NH ₃ -N							
C. Tertiary treatment - description:							
BOD ₅							
TSS							
NH ₃ -N							
Plant Effluent -							
CBOD ₅	25	10					
TSS	38	15					
NH ₃ -N							

IOWA DEPARTMENT OF WATER, AIR AND WASTE MANAGEMENT

WATER QUALITY PROGRAM		CONSTRUCTION PERMIT APPLICATION SCHEDULE K2, AERATED POND		WAWM USE																																																																																																																																															
DATE PREPARED February 5, 1988	PROJECT IDENTITY City of Long Grove Treatment System Improvements		PROJECT NO.																																																																																																																																																
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<p>1. Design Basis:</p> <table style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 30%;"></th> <th style="width: 20%; text-align: center;">AWW</th> <th style="width: 20%; text-align: center;">MWW</th> <th style="width: 30%; text-align: center;">PHWW</th> </tr> </thead> <tbody> <tr> <td>Flow, MGD</td> <td style="text-align: center;">.060</td> <td style="text-align: center;">.090</td> <td style="text-align: center;">.090</td> </tr> <tr> <td>BOD₅, #/day</td> <td style="text-align: center;">85</td> <td style="text-align: center;">85</td> <td style="text-align: center;">85</td> </tr> </tbody> </table> <p>2. No. of soil borings taken <u>NA</u>. Data included in the _____.</p> <p>High groundwater elevation (MSL) <u>713.18</u>.</p> <p>3. Top of dike elevation (MSL) <u>736.5</u> ft. 100 year flood elevation (MSL) <u>NA</u> ft.</p> <p>4. Pond Data</p> <table style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 35%;"></th> <th style="width: 12.5%; text-align: center;">Cell 1</th> <th style="width: 12.5%; text-align: center;">Cell 2</th> <th style="width: 12.5%; text-align: center;">Cell 3</th> <th style="width: 12.5%; text-align: center;">Cell 4</th> <th style="width: 15%; text-align: center;">Total</th> </tr> </thead> <tbody> <tr> <td>Surface area @ maximum depth (A)</td> <td style="text-align: center;">.28</td> <td style="text-align: center;">.31</td> <td style="text-align: center;">1.32</td> <td></td> <td></td> </tr> <tr> <td>Maximum operation depth (ft)</td> <td style="text-align: center;">6.00</td> <td style="text-align: center;">6.00</td> <td style="text-align: center;">6.00</td> <td></td> <td></td> </tr> <tr> <td>Minimum operation depth (ft)</td> <td style="text-align: center;">6.00</td> <td style="text-align: center;">6.00</td> <td style="text-align: center;">6.00</td> <td></td> <td></td> </tr> <tr> <td>Effective storage volume (MG)</td> <td style="text-align: center;">.87</td> <td style="text-align: center;">.87</td> <td style="text-align: center;">2.73</td> <td></td> <td></td> </tr> <tr> <td>Effective detention time (days)</td> <td style="text-align: center;">14.5</td> <td style="text-align: center;">14.5</td> <td style="text-align: center;">43</td> <td></td> <td></td> </tr> <tr> <td colspan="6">Air Requirements:</td> </tr> <tr> <td>Provided (ft³/#BOD)</td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>Provided (#O₂/#BOD)</td> <td style="text-align: center;">3.4</td> <td style="text-align: center;">4.2</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Required (#O₂/#BOD)</td> <td style="text-align: center;">2</td> <td style="text-align: center;">2</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Minimum D.O. level (mg/l)</td> <td style="text-align: center;">2</td> <td style="text-align: center;">2</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Freeboard @ maximum depth (ft)</td> <td style="text-align: center;">2.75</td> <td style="text-align: center;">2.75</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Top width of dike (ft)</td> <td style="text-align: center;">10</td> <td style="text-align: center;">10</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Inner embankment slope H/V</td> <td style="text-align: center;">3/1</td> <td style="text-align: center;">3/1</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Outer embankment slope H/V</td> <td style="text-align: center;">3/1</td> <td style="text-align: center;">3/1</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Type of Inlet</td> <td colspan="3" style="text-align: center;">Submerged---</td> <td></td> <td></td> </tr> <tr> <td>Top drawoff level (ft)</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> <td></td> <td></td> </tr> <tr> <td>Middle drawoff level (ft)</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">3'</td> <td></td> <td></td> </tr> <tr> <td>Bottom drawoff level (ft)</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">4'</td> <td></td> <td></td> </tr> </tbody> </table> <p>5. Aeration Equipment: Design Air Temperature <u>NA</u> °F to _____ °F.</p> <p>Type <u>Floating</u>. Manufacturer & Model <u>Environmental Equipment Eng.</u></p> <p>No. of Units <u>3</u>. HP or CFM/unit <u>3 Hp</u> Total HP or CFM <u>9 Hp</u></p> <p>K value <u>.06</u> /day at design temperature <u>1</u> °C.</p> <p>Is a layout of the aeration system given on Schedule H1? Yes <u>X</u> No _____</p> <p>6. Is cold weather protection provided? Yes _____ How? <u>Submerged motors and props</u></p> <p>7. Method of raw flow diversion to cells <u>NA</u></p> <p>8. Method of interconnection of cells <u>Floating Baffle Wall Windows</u></p> <p>9. Provision to prevent drawoff of floating solids <u>Submerged outlets</u></p> <p>10. Method of sampling <u>Manual</u></p> <p>11. Type of flow measurement <u>sonic</u> Location <u>@ 90° V notch weir @ influent</u></p> <p>12. Fence Height <u>6'</u> No. strands of barbed wire: Top _____ Bottom _____</p> <p>13. Number of warning signs <u>5</u>. Location <u>Along boundary fence</u></p> <p>14. Will pond be pre-filled to 2 ft. level? Yes _____ No _____ <u>NA</u></p> <p>15. Maximum allowable leakage rate <u>NA</u> in/day.</p> <p>Method of testing leakage rate <u>NA</u></p> <p>16. Are specifications included for:</p> <table style="width: 100%; border-collapse: collapse;"> <tbody> <tr> <td style="width: 50%;">a. Seeding</td> <td style="width: 10%;">Yes _____</td> <td style="width: 10%;">No <u>X</u></td> <td rowspan="5" style="width: 10%; vertical-align: middle; font-size: 3em;">}</td> <td rowspan="5" style="width: 10%; vertical-align: middle;">NA</td> </tr> <tr> <td>b. Soil sterilization</td> <td>Yes _____</td> <td>No <u>X</u></td> </tr> <tr> <td>c. Pond bottom uniformity</td> <td>Yes _____</td> <td>No <u>X</u></td> </tr> <tr> <td>d. Pond sealing</td> <td>Yes _____</td> <td>No <u>X</u></td> </tr> <tr> <td>e. Erosion protection</td> <td>Yes _____</td> <td>No <u>X</u></td> </tr> </tbody> </table> <p>17. Is service bypass provided? <u>No</u> Discharge to _____</p>						AWW	MWW	PHWW	Flow, MGD	.060	.090	.090	BOD ₅ , #/day	85	85	85		Cell 1	Cell 2	Cell 3	Cell 4	Total	Surface area @ maximum depth (A)	.28	.31	1.32			Maximum operation depth (ft)	6.00	6.00	6.00			Minimum operation depth (ft)	6.00	6.00	6.00			Effective storage volume (MG)	.87	.87	2.73			Effective detention time (days)	14.5	14.5	43			Air Requirements:						Provided (ft ³ /#BOD)						Provided (#O ₂ /#BOD)	3.4	4.2				Required (#O ₂ /#BOD)	2	2				Minimum D.O. level (mg/l)	2	2				Freeboard @ maximum depth (ft)	2.75	2.75				Top width of dike (ft)	10	10				Inner embankment slope H/V	3/1	3/1				Outer embankment slope H/V	3/1	3/1				Type of Inlet	Submerged---					Top drawoff level (ft)	NA	NA	NA			Middle drawoff level (ft)	NA	NA	3'			Bottom drawoff level (ft)	NA	NA	4'			a. Seeding	Yes _____	No <u>X</u>	}	NA	b. Soil sterilization	Yes _____	No <u>X</u>	c. Pond bottom uniformity	Yes _____	No <u>X</u>	d. Pond sealing	Yes _____	No <u>X</u>	e. Erosion protection	Yes _____	No <u>X</u>
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